

SNS Linac Technical Memo

Faraday Cup Outgassing Rate

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4/4/2001

WBS 1.4.5.2.? (Diagnostics – Faraday Cup)

Vacuum Loads for SNS Faraday Cup

Summary : In order to do the initial design of the D-plate vacuum system a calculation was done to estimate the out-gassing load from the Faraday Cup. The Faraday Cup for the D-plate is being developed under WBS 1.4.5.2.?, since it will be used elsewhere in the accelerator. Also note that as the designs of these devices become more mature, the responsible person should update these values and pass the information on to the vacuum system designers, especially if the new values exceed these presented here.

The assumptions made were:

Device is mounted on a linear actuator similar to the wirescanner.

Kapton insulated wires are used to bring the signals out from the vacuum.

Copper water cooling lines are also used.

Conclusion

The estimated out-gassing rate for the Faraday Cup is 1.835×10^{-7} torr*L/s

Inner surfaces exposed to vacuum:

$$d := 3 \cdot \text{cm}$$

$$d = 1.18 \text{ in}$$

$$t_{\text{foil}} := .0025 \cdot \text{in}$$

$$t_{\text{cup}} := 0.013 \text{ in}$$

$$C_{\text{cup}} := \frac{\pi \cdot d^2}{4} + \pi d \cdot t_{\text{cup}}$$

$$C_{\text{cup}} = 7.38 \text{ cm}^2$$

$$t_{\text{plate}} := 0.25 \cdot \text{in}$$

$$Cu_{plate} := \frac{\pi \cdot d^2}{4} + \pi d \cdot t_{plate}$$

$$Cu_{plate} = 13.053 \text{ cm}^2$$

Estimate the amount of copper tubing exposed to the vacuum

$$d_{tubing} := 0.25 \cdot \text{in}$$

$$L_{tubing} := 36 \cdot \text{in}$$

$$Cu_{tubing} := \pi \cdot d_{tubing} \cdot L_{tubing}$$

$$Cu_{tubing} = 182.415 \text{ cm}^2$$

$$Cu_{total} := Cu_{plate} + Cu_{tubing}$$

$$Cu_{total} = 195.468 \text{ cm}^2$$

Signal wires, assuming .024" diameter Kapton insulated wires.

$$Wire_{SA} := 6 \cdot 24 \cdot \text{in} \cdot \pi \cdot .024 \cdot \text{in}$$

$$Wire_{SA} = 70.047 \text{ cm}^2$$

$$Wire_{SA} = 10.857 \text{ in}^2$$

The following values are based on a design similar to the wire scanner.

$$Guide_rail_{SA} := 19.91 \text{ in}^2$$

$$Guide_rail_{SA} = 128.451 \text{ cm}^2$$

$$Support_{SA} := 84.1 \text{ in}^2$$

$$Support_{SA} = 542.58 \text{ cm}^2$$

$$Tube_{SA} := \pi \cdot (.625 \cdot \text{in} + .375 \cdot \text{in}) \cdot 14.2 \text{ in}$$

$$Tube_{SA} = 287.81 \text{ cm}^2$$

$$Bellows_{SA} := \frac{\pi}{4} \cdot \left[(2.2 \cdot \text{in})^2 - (1.04 \text{ in})^2 \right] \cdot 122$$

$$Bellows_{SA} = 457.058 \text{ cm}^2$$

$$Box_{SA} := \pi \cdot 1.5 \text{ in} \cdot 3 \text{ in}$$

$$Box_{SA} = 91.207 \text{ cm}^2$$

Outgassing rate of exposed surfaces

$$LR_{ss} := 1 \cdot 10^{-10} \cdot \frac{\text{torr} \cdot L}{s \cdot \text{cm}^2}$$

$$LR_{Cu} := LR_{ss}$$

$$LR_C := 1.736 \cdot 10^{-8} \cdot \frac{\text{torr} \cdot L}{s \cdot \text{cm}^2}$$

Total outgassing of stainless and copper parts is:

$$OGR_{ss} := LR_{ss} \cdot (Cu_{\text{total}} + \text{Guide_rail}_{SA} + \text{Support}_{SA} + \text{Tube}_{SA} + \text{Bellows}_{SA} + \text{Box}_{SA})$$

$$OGR_{ss} = 1.703 \times 10^{-7} \frac{\text{torr} \cdot L}{s}$$

Outgassing rate as measured by Virgo

$$LR_{\text{kapton}} := 8.36 \cdot 10^{-11} \cdot \frac{\text{torr} \cdot L}{s \cdot \text{cm}^2}$$

$$OGR_{\text{kapton}} := \text{Wire}_{SA} \cdot LR_{\text{kapton}}$$

$$OGR_{\text{kapton}} = 5.856 \times 10^{-9} \frac{\text{torr} \cdot L}{s}$$

Seals and their leak rates

$$\text{Bellows} := 2 \cdot 10^{-9} \cdot \frac{\text{torr} \cdot L}{s}$$

$$\text{conflat} := 1 \cdot 10^{-10} \cdot \text{torr} \cdot \frac{L}{s}$$

$$\text{viton} := 5 \cdot 10^{-9} \cdot \text{torr} \cdot \frac{L}{s}$$

Total leak rate of the faraday cup is:

$$OGR_{FC} := OGR_{ss} + \text{Bellows} + 4 \cdot \text{conflat} + \text{viton} + OGR_{\text{kapton}}$$

$$OGR_{FC} = 1.835 \times 10^{-7} \frac{\text{torr} \cdot L}{s}$$